

Exercise A2

Problem 1

Let's consider a 1800 MHz public mobile radio system operating in a microcellular environment. The base station is at a height of 3 m above the ground and the mobile at 1 m. The antenna gains are 5 and 3 dBi's for the BS and the mobile antenna, respectively.

It is required to determine the minimum transmitted power in order for the BS to serve a mobile at a distance of 1000 m in LOS. Receiver sensitivity is -104 dBm. Ground reflection must be taken into account.

Problem 2

Now the mobile turns into a perpendicular street and goes another 100 meters down the street. The same minimum Tx power as in problem 1 must be determined, this time neglecting ground reflection, assuming the same height for both terminals and using GTD diffraction coefficients. Both the BS and the mobile are at 10 m from the side of the street. Polarization is horizontal.

Solution

Problem 1

Friis's equation is:

$$P_t(\text{dBm}) = P_r(\text{dBm}) - G_t - G_r + 20 \cdot \log(4\pi d/\lambda)$$

If only the direct ray is considered we have

$$P_t'(\text{dBm}) = -104 - 5 - 3 + 97.6 = -14.4 \text{ dBm}$$

If also ground reflection is considered we have an additional path gain of

$$20 \cdot \log \left\{ \frac{|E|}{|E_0|} \right\} = 20 \cdot \log \left\{ 2 \left| \sin \left(\frac{2\pi}{\lambda} \frac{h_1 h_2}{d} \right) \right| \right\} = -13.15 \text{ dB}$$

Since link distance is much greater than breakpoint distance (about 72 m here) also the simplified formula could be used:

$$20 \cdot \log \left\{ \frac{|E|}{|E_0|} \right\} = 20 \cdot \log \left\{ \frac{4\pi}{\lambda} \frac{h_1 h_2}{d} \right\} = -12.91 \text{ dB}$$

Using the first, more accurate result we get:

$$P_t(\text{dBm}) = P_t' + 13.15 = -0.9 \text{ dBm}$$

Problem 2

Adopting a similar approach as before, if diffraction would cause no attenuation we'd have a total path of

$$s' + s = \sqrt{1000^2 + 10^2} + \sqrt{100^2 + 10^2} \approx 1000 + 100.5 = 1100.5 \text{ m}$$

Without diffraction we would therefore get:

$$P_t'(\text{dBm}) = -104 - 5 - 3 + 98.4 = -13.6 \text{ dBm}$$

Now let's derive the additional path gain with diffraction

$$PG = 20 * \text{Log} \left\{ \frac{|E|}{|E_0|} \right\}$$

The field of the unfolded ray without diffraction would be

$$\mathbf{E}_0 = j \sqrt{\frac{\eta PG_{Tx}}{2\pi}} \frac{e^{-j\beta r}}{r} \mathbf{i}_x = j \sqrt{60EIRP} \frac{e^{-j\beta r}}{r} \mathbf{i}_x$$

Thus:

$$|\mathbf{E}_0| = \frac{\sqrt{60EIRP}}{s+s'} \quad (1)$$

Where $s+s'$ is the total unfolded ray length. Now, if P_d is the diffraction point on the edge, for the diffracted field we have:

$$|E| = |E(P_d)| \cdot |D| \cdot A(s, s') = \frac{\sqrt{60EIRP}}{s'} |D_H| \cdot \sqrt{\frac{s'}{s(s+s')}}$$

Therefore (see also the appendix)

$$PG = 20 * \text{Log} \left\{ \frac{|E|}{|E_0|} \right\} = 20 * \text{Log} \left\{ |D_H| \cdot \frac{s+s'}{s'} \sqrt{\frac{s'}{s(s+s')}} \right\} =$$

$$20 * \text{Log} \left\{ |D_H| \cdot \sqrt{\frac{s+s'}{s \cdot s'}} \right\} \approx -36.06 \text{ dB}$$

And transmitted power must be

$$P_t = P_t' + 36.06 = -13.6 + 36.06 \approx 22.5 \text{ dBm} \approx 178 \text{ mW}$$

A more straightforward method is to compute the field at the diffraction point using a formula similar to (1), then compute the diffracted field in the destination point with the usual GTD formula, and finally derive the received power (as a function of the Tx power) by multiplying the destination incident power density by the effective area of the Rx antenna.

Adopting this approach we have:

$$|E| = |E(P_d)| \cdot |D| \cdot A(s, s') = \frac{\sqrt{60EIRP}}{s'} |D_H| \cdot \sqrt{\frac{s'}{s(s+s')}}$$

where

$$A(s, s') = \sqrt{\frac{s'}{s(s+s')}} = 0.095 \quad \text{and} \quad |D_H| = 0.15$$

therefore:

$$P_R = \frac{|E|^2}{2\eta} G_R \frac{\lambda^2}{4\pi} = -104 \text{ [dBm]} = 39.8 \times 10^{-15} \text{ [W]}$$

Thus :

$$|E|^2 = P_R \frac{2\eta \cdot 4\pi}{G_R \cdot \lambda^2} = P_R \frac{8 \cdot 120\pi^2}{G_R \cdot \lambda^2}$$

↓

$$\frac{\sqrt{60EIRP}}{s'} |D_H| \cdot A = \sqrt{P_R \frac{8 \cdot 120\pi^2}{G_R \cdot \lambda^2}}$$

↓

$$EIRP = P_R \frac{8 \cdot 2\pi^2}{G_R \cdot \lambda^2} \frac{s'^2}{|D_H|^2 \cdot A^2}$$

↓

$$P_T = P_R \frac{8 \cdot 2\pi^2}{G_T G_R \cdot \lambda^2} \frac{s'^2}{|D_H|^2 \cdot A^2} = 39.8 \times 10^{-15} \frac{16\pi^2}{3.16 \cdot 2 \cdot \lambda^2} \frac{1000^2}{0.15^2 \cdot 0.095^2} = 0.177 \text{ [W]}$$

Appendix: computation of $|D_H|$

The GTD expression is:

$$D^H(\phi, \phi', n) = \frac{-e^{-j\pi/4} \cdot \sin(\pi/n)}{n\sqrt{2\pi\beta}} \cdot \left[\frac{1}{\cos(\pi/n) - \cos(\xi^-/n)} + \frac{1}{\cos(\pi/n) - \cos(\xi^+/n)} \right] \quad (1)$$

In this case:

$$n = 1.5$$

$$\phi = 1.5\pi - \text{atan}(10/100) = 4.61 \text{ Rad}$$

$$\phi' = \text{atan}(10/1000) = 0.01$$

$$\zeta^- = \phi - \phi' = 4.6$$

$$\zeta^+ = \phi + \phi' = 4.62$$

The square parenthesis in 1) gives therefore

$$\left[\frac{1}{\cos(\pi/1.5) - \cos(4.60/1.5)} + \frac{1}{\cos(\pi/1.5) - \cos(4.62/1.5)} \right] = [2.01 + 2.008] = 4.018$$

While the preceding factor gives:

$$\left| \frac{-e^{-j\pi/4} \cdot \sin(\pi/n)}{n\sqrt{2\pi\beta}} \right| = \frac{\sin(\pi/1.5) \overline{\lambda}}{1.5 \cdot 2\pi} = 0.037$$

Thus:

$$|D^H| = 0.037 \cdot 4.018 = 0.15$$

